

## Specifier's comments:

## 1 Input data

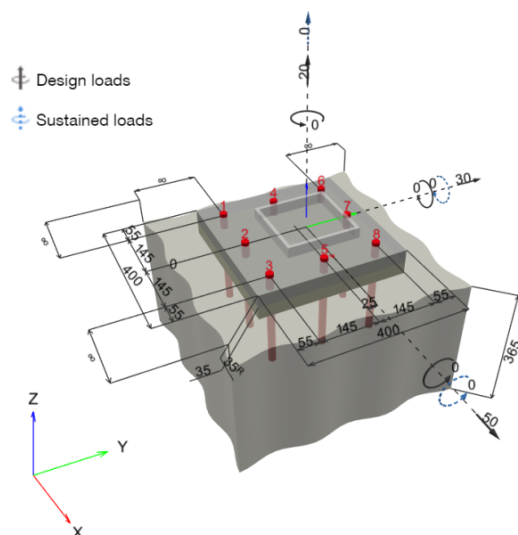
<b>Anchor type and size:</b>	<b>HIT-HY 200-A + HAS-U A4 M20</b>
Return period (service life in years):	50
Item number:	2223929 HAS-U A4 M20x350 (insert) / 2022696 HIT-HY 200-A (mortar)
Effective embedment depth:	$h_{ef,act} = 200.0 \text{ mm}$ ( $h_{ef,limit} = - \text{mm}$ )
Material:	A4
Approval No.:	ETA 11/0493
Issued I Valid:	30/08/2019   -
Proof:	Design Method EN 1992-4, Chemical
Stand-off installation:	without clamping (anchor); restraint level (baseplate): 2.00; $e_b = 35.0 \text{ mm}$ ; $t = 35.0 \text{ mm}$  Hilti Grout: , multipurpose, $f_{c,Grout} = 30.00 \text{ N/mm}^2$ Baseplate <sup>R</sup> : $l_x \times l_y \times t = 400.0 \text{ mm} \times 400.0 \text{ mm} \times 35.0 \text{ mm}$ ; (Recommended plate thickness: not calculated) Profile: Square hollow, 200 x 200 x 10,0; (L x W x T) = 200.0 mm x 200.0 mm x 10.0 mm Base material: cracked concrete, C40/50, $f_{c,cyl} = 40.00 \text{ N/mm}^2$ ; $h = 365.0 \text{ mm}$ , Temp. short/long: 0/0 °C <b>Installation:</b> <b>hammer drilled hole, Installation condition: Dry</b> Reinforcement: No reinforcement or Reinforcement spacing $\geq 150 \text{ mm}$ (any $\emptyset$ ) or $\geq 100 \text{ mm}$ ( $\emptyset \leq 10 \text{ mm}$ ) no longitudinal edge reinforcement



**Application also possible with HVU2 + HAS-U A4 M20 under the selected boundary conditions.**  
**More information in section Alternative fastening data of this report.**

<sup>R</sup> - The anchor calculation is based on a rigid baseplate assumption.

## Geometry [mm] & Loading [kN, kNm]



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## 1.1 Load combination

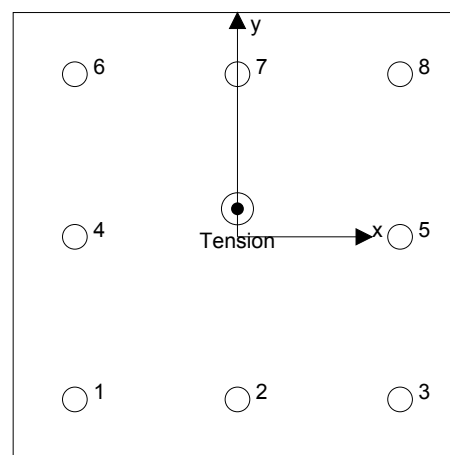
Case	Description	Forces [kN] / Moments [kNm]	Seismic	Fire	Max. Util. Anchor [%]
1	Combination 1	$N = 20.000; V_x = 50.000; V_y = 30.000;$ $M_x = 0.000; M_y = 0.000; M_z = 0.000;$ $N_{sus} = 0.000; M_{x,sus} = 0.000; M_{y,sus} = 0.000;$	no	no	92

## 2 Load case/Resulting anchor forces

### Anchor reactions [kN]

Tension force: (+Tension, -Compression)

Anchor	Tension force	Shear force	Shear force x	Shear force y
1	1.925	7.111	5.532	4.468
2	1.925	6.683	5.532	3.750
3	1.925	6.308	5.532	3.032
4	2.500	7.683	6.250	4.468
5	2.500	6.946	6.250	3.032
6	3.075	8.278	6.968	4.468
7	3.075	7.913	6.968	3.750
8	3.075	7.599	6.968	3.032



max. concrete compressive strain:

- [%]

max. concrete compressive stress:

- [N/mm<sup>2</sup>]

resulting tension force in (x/y)=(0.0/25.0):

20.000 [kN]

resulting compression force in (x/y)=(0.0/0.0):

0.000 [kN]

Anchor forces are calculated based on the assumption of a rigid baseplate.

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### 3 Tension load (EN 1992-4, Section 7.2.1)

	Load [kN]	Capacity [kN]	Utilization $\beta_N$ [%]	Status
Steel failure*	3.075	91.711	4	OK
Combined pullout-concrete cone failure**	20.000	190.094	11	OK
Concrete Breakout failure**	20.000	186.505	11	OK
Splitting failure**	N/A	N/A	N/A	N/A

\* highest loaded anchor    \*\*anchor group (anchors in tension)

#### 3.1 Steel failure

$$N_{Ed} \leq N_{Rd,s} = \frac{N_{Rk,s}}{\gamma_{M,s}} \quad \text{EN 1992-4, Table 7.1}$$

$N_{Rk,s}$ [kN]	$\gamma_{M,s}$	$N_{Rd,s}$ [kN]	$N_{Ed}$ [kN]
171.500	1.870	91.711	3.075

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### 3.2 Combined pullout-concrete cone failure

$$N_{Ed} \leq N_{Rd,p} = \frac{N_{Rk,p}}{\gamma_{M,p}} \quad \text{EN 1992-4, Table 7.1}$$

$$N_{Rk,p} = N_{Rk,p}^0 \cdot \frac{A_{p,N}}{A_{p,N}^0} \cdot \psi_{g,Np} \cdot \psi_{s,Np} \cdot \psi_{re,N} \cdot \psi_{ec1,Np} \cdot \psi_{ec2,Np} \quad \text{EN 1992-4, Eq. (7.13)}$$

$$N_{Rk,p}^0 = \psi_{sus} \cdot \tau_{Rk} \cdot \pi \cdot d \cdot h_{ef} \quad \text{EN 1992-4, Eq. (7.14)}$$

$$\psi_{sus} = 1 \quad \text{EN 1992-4, Eq. (7.14a)}$$

$$s_{cr,Np} = 7.3 \cdot d \cdot \sqrt{\psi_{sus} \cdot \tau_{Rk}} \leq 3 \cdot h_{ef} \quad \text{EN 1992-4, Eq. (7.15)}$$

$$\psi_{g,Np} = \psi_{g,Np}^0 - \left( \frac{s}{s_{cr,Np}} \right)^{0.5} \cdot (\psi_{g,Np}^0 - 1) \geq 1.00 \quad \text{EN 1992-4, Eq. (7.17)}$$

$$\psi_{g,Np}^0 = \sqrt{n} - (\sqrt{n} - 1) \cdot \left( \frac{\tau_{Rk}}{\tau_{Rk,c}} \right)^{1.5} \geq 1.00 \quad \text{EN 1992-4, Eq. (7.18)}$$

$$\tau_{Rk,c} = \frac{k_3}{\pi \cdot d} \cdot \sqrt{h_{ef} \cdot f_{ck}} \quad \text{EN 1992-4, Eq. (7.19)}$$

$$\psi_{s,Np} = 0.7 + 0.3 \cdot \frac{c}{c_{cr,Np}} \leq 1.00 \quad \text{EN 1992-4, Eq. (7.20)}$$

$$\psi_{ec1,Np} = \frac{1}{1 + \left( \frac{2 \cdot e_{c1,N}}{s_{cr,Np}} \right)} \leq 1.00 \quad \text{EN 1992-4, Eq. (7.21)}$$

$$\psi_{ec2,Np} = \frac{1}{1 + \left( \frac{2 \cdot e_{c2,N}}{s_{cr,Np}} \right)} \leq 1.00 \quad \text{EN 1992-4, Eq. (7.21)}$$

$A_{p,N}$ [mm <sup>2</sup> ]	$A_{p,N}^0$ [mm <sup>2</sup> ]	$\tau_{Rk,ucr,20}$ [N/mm <sup>2</sup> ]	$s_{cr,Np}$ [mm]	$c_{cr,Np}$ [mm]	$c_{min}$ [mm]	$f_{c,cyl}$ [N/mm <sup>2</sup> ]
792,100	360,000	18.00	600.0	300.0	∞	40.00
$\psi_c$	$\tau_{Rk,cr}$ [N/mm <sup>2</sup> ]	$k_3$	$\tau_{Rk,c}$ [N/mm <sup>2</sup> ]	$\psi_{g,Np}^0$	$\psi_{g,Np}$	
1.079	9.17	7.700	10.96	1.429	1.218	
$e_{c1,N}$ [mm]	$\psi_{ec1,Np}$	$e_{c2,N}$ [mm]	$\psi_{ec2,Np}$	$\psi_{s,Np}$	$\psi_{re,Np}$	
0.0	1.000	25.0	0.923	1.000	1.000	
$\psi_{sus}^0$	$\alpha_{sus}$	$\psi_{sus}$				
0.740	0.000	1.000				
$N_{Rk,p}^0$ [kN]	$N_{Rk,p}$ [kN]	$\gamma_{M,p}$	$N_{Rd,p}$ [kN]	$N_{Ed}$ [kN]		
115.277	285.141	1.500	190.094	20.000		

Group anchor ID

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### 3.3 Concrete Breakout failure

$$N_{Ed} \leq N_{Rd,c} = \frac{N_{Rk,c}}{\gamma_{M,c}} \quad \text{EN 1992-4, Table 7.1}$$

$$N_{Rk,c} = N_{Rk,c}^0 \cdot \frac{A_{c,N}}{A_{c,N}^0} \cdot \psi_{s,N} \cdot \psi_{re,N} \cdot \psi_{ec1,N} \cdot \psi_{ec2,N} \cdot \psi_{M,N} \quad \text{EN 1992-4, Eq. (7.1)}$$

$$N_{Rk,c}^0 = k_1 \cdot \sqrt{f_{ck}} \cdot h_{ef}^{1.5} \quad \text{EN 1992-4, Eq. (7.2)}$$

$$A_{c,N}^0 = s_{cr,N} \cdot s_{cr,N} \quad \text{EN 1992-4, Eq. (7.3)}$$

$$\psi_{s,N} = 0.7 + 0.3 \cdot \frac{c}{c_{cr,N}} \leq 1.00 \quad \text{EN 1992-4, Eq. (7.4)}$$

$$\psi_{ec1,N} = \frac{1}{1 + \left( \frac{2 \cdot e_{N,1}}{s_{cr,N}} \right)} \leq 1.00 \quad \text{EN 1992-4, Eq. (7.6)}$$

$$\psi_{ec2,N} = \frac{1}{1 + \left( \frac{2 \cdot e_{N,2}}{s_{cr,N}} \right)} \leq 1.00 \quad \text{EN 1992-4, Eq. (7.6)}$$

$$\psi_{M,N} = 1 \quad \text{EN 1992-4, Eq. (7.7)}$$

$A_{c,N} [\text{mm}^2]$	$A_{c,N}^0 [\text{mm}^2]$	$c_{cr,N} [\text{mm}]$	$s_{cr,N} [\text{mm}]$	$f_{c,cyl} [\text{N/mm}^2]$		
792,100	360,000	300.0	600.0	40.00		
$e_{c1,N} [\text{mm}]$	$\psi_{ec1,N}$	$e_{c2,N} [\text{mm}]$	$\psi_{ec2,N}$	$\psi_{s,N}$	$\psi_{re,N}$	
0.0	1.000	25.0	0.923	1.000	1.000	
$z [\text{mm}]$	$\psi_{M,N}$	$k_1$	$N_{Rk,c}^0 [\text{kN}]$	$\gamma_{M,c}$	$N_{Rd,c} [\text{kN}]$	$N_{Ed} [\text{kN}]$
0.0	1.000	7.700	137.742	1.500	186.505	20.000
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## 4 Shear load (EN 1992-4, Section 7.2.2)

	Load [kN]	Capacity [kN]	Utilization $\beta_v$ [%]	Status
Steel failure (without lever arm)*	8.278	55.000	16	OK
Steel failure (with lever arm)*	8.278	9.009	92	OK
Pryout failure**	58.310	367.260	16	OK
Concrete edge failure in direction **	N/A	N/A	N/A	N/A

\* highest loaded anchor    \*\*anchor group (relevant anchors)

### 4.1 Steel failure (without lever arm)

$$V_{Ed} \leq V_{Rd,s} = \frac{V_{Rk,s}}{\gamma_{M,s}} \quad \text{EN 1992-4, Table 7.2}$$

$$V_{Rk,s} = k_7 \cdot V_{Rk,s}^0 \quad \text{EN 1992-4, Eq. (7.35)}$$

$V_{Rk,s}^0$ [kN]	$k_7$	$V_{Rk,s}$ [kN]	$\gamma_{M,s}$	$V_{Rd,s}$ [kN]	$V_{Ed}$ [kN]
85.800	1.000	85.800	1.560	55.000	8.278

### 4.2 Steel failure (with lever arm)

$$V_{Ed} \leq V_{Rd,s,M} = \frac{V_{Rk,s,M}}{\gamma_{M,s}} \quad \text{EN 1992-4, Table 7.2}$$

$$V_{Rk,s,M} = \frac{\alpha_M \cdot M_{Rk,s}}{l_a} \quad \text{EN 1992-4, Eq. 7.37}$$

$$M_{Rk,s} = M_{Rk,s}^0 \cdot \left(1 - \frac{N_{Ed}}{N_{Rd,s}}\right) \quad \text{EN 1992-4, Eq. 7.38}$$

$$l_a = e_c + \frac{t}{2} + a_3 \quad \text{EN 1992-4, Eq. 6.2}$$

$l$ [mm]	$\alpha_M$			
62.5	2.00			
$N_{Ed} / N_{Rd,s}$	$1 - N_{Ed} / N_{Rd,s}$	$M_{Rk,s}^0$ [kNm]	$M_{Rk,s} = M_{Rk,s}^0 (1 - N_{Ed} / N_{Rd,s})$ [kNm]	
0.034	0.966	0.454	0.439	
$V_{Rk,s}^M = \alpha_M \cdot M_{Rk,s} / l$ [kN]		$\gamma_{M,s}$	$V_{Rd,s}^M$ [kN]	$V_{Ed}$ [kN]
14.053		1.560	9.009	8.278

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### 4.3 Pryout failure (concrete cone relevant)

$$V_{Ed} \leq V_{Rd,cp} = \frac{V_{Rk,cp}}{\gamma_{M,c,p}} \quad \text{EN 1992-4, Table 7.2}$$

$$V_{Rk,cp} = k_8 \cdot \min \{N_{Rk,c}^0; N_{Rk,p}\} \quad \text{EN 1992-4, Eq. (7.39c)}$$

$$N_{Rk,c}^0 = N_{Rk,c}^0 \cdot \frac{A_{c,N}}{A_{c,N}^0} \cdot \psi_{s,N} \cdot \psi_{re,N} \cdot \psi_{ec1,N} \cdot \psi_{ec2,N} \cdot \psi_{M,N} \quad \text{EN 1992-4, Eq. (7.1)}$$

$$N_{Rk,c}^0 = k_1 \cdot \sqrt{f_{ck}} \cdot h_{ef}^{1.5} \quad \text{EN 1992-4, Eq. (7.2)}$$

$$A_{c,N}^0 = s_{cr,N} \cdot s_{cr,N} \quad \text{EN 1992-4, Eq. (7.3)}$$

$$\psi_{s,N} = 0.7 + 0.3 \cdot \frac{c}{c_{cr,N}} \leq 1.00 \quad \text{EN 1992-4, Eq. (7.4)}$$

$$\psi_{ec1,N} = \frac{1}{1 + \left( \frac{2 \cdot e_{V,1}}{s_{cr,N}} \right)} \leq 1.00 \quad \text{EN 1992-4, Eq. (7.6)}$$

$$\psi_{ec2,N} = \frac{1}{1 + \left( \frac{2 \cdot e_{V,2}}{s_{cr,N}} \right)} \leq 1.00 \quad \text{EN 1992-4, Eq. (7.6)}$$

$$\psi_{M,N} = 1 \quad \text{EN 1992-4, Eq. (7.7)}$$

$A_{c,N}$ [mm <sup>2</sup> ]	$A_{c,N}^0$ [mm <sup>2</sup> ]	$c_{cr,N}$ [mm]	$s_{cr,N}$ [mm]	$k_8$	$f_{c,cyl}$ [N/mm <sup>2</sup> ]	
792,100	360,000	300.0	600.0	2.000	40.00	
$e_{c1,V}$ [mm]	$\psi_{ec1,N}$	$e_{c2,V}$ [mm]	$\psi_{ec2,N}$	$\psi_{s,N}$	$\psi_{re,N}$	$\psi_{M,N}$
11.0	0.965	18.4	0.942	1.000	1.000	1.000
$k_1$	$N_{Rk,c}^0$ [kN]	$\gamma_{M,c,p}$	$V_{Rd,cp}$ [kN]	$V_{Ed}$ [kN]		
7.700	137.742	1.500	367.260	58.310		
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## 5 Combined tension and shear loads (EN 1992-4, Section 7.2.3)

Steel failure

$\beta_N$	$\beta_V$	$\alpha$	Utilization $\beta_{N,V}$ [%]	Status
0.034	0.151	2.000	3	OK

$$\beta_N^\alpha + \beta_V^\alpha \leq 1.0$$

Concrete failure

$\beta_N$	$\beta_V$	$\alpha$	Utilization $\beta_{N,V}$ [%]	Status
0.107	0.159	1.500	10	OK

$$\beta_N^\alpha + \beta_V^\alpha \leq 1.0$$

## 6 Displacements (highest loaded anchor)

Short term loading:

$N_{Sk}$	=	2.278 [kN]	$\delta_N$	=	0.0127 [mm]
$V_{Sk}$	=	6.132 [kN]	$\delta_V$	=	0.2453 [mm]
			$\delta_{NV}$	=	0.2456 [mm]

Long term loading:

$N_{Sk}$	=	2.278 [kN]	$\delta_N$	=	0.0290 [mm]
$V_{Sk}$	=	6.132 [kN]	$\delta_V$	=	0.3679 [mm]
			$\delta_{NV}$	=	0.3691 [mm]

Comments: Tension displacements are valid with half of the required installation torque moment for uncracked concrete! Shear displacements are valid without friction between the concrete and the baseplate! The gap due to the drilled hole and clearance hole tolerances are not included in this calculation!

The acceptable anchor displacements depend on the fastened construction and must be defined by the designer!



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## 7 Warnings

- The anchor design methods in PROFIS Engineering require rigid baseplates per current regulations (AS 5216:2018, ETAG 001/Annex C, EOTA TR029 etc.). This means load re-distribution on the anchors due to elastic deformations of the baseplate are not considered - the baseplate is assumed to be sufficiently stiff, in order not to be deformed when subjected to the design loading. PROFIS Engineering calculates the minimum required baseplate thickness with CBFEM to limit the stress of the baseplate based on the assumptions explained above. The proof if the rigid baseplate assumption is valid is not carried out by PROFIS Engineering. Input data and results must be checked for agreement with the existing conditions and for plausibility!
- Checking the transfer of loads into the base material is required in accordance with EN 1992-4, Annex A!
- The design is only valid if the clearance hole in the fixture is not larger than the value given in Table 6.1 of EN 1992-4! For larger diameters of the clearance hole see section 6.2.2 of EN 1992-4!
- The accessory list in this report is for the information of the user only. In any case, the instructions for use provided with the product have to be followed to ensure a proper installation.
- For the determination of the  $\psi_{re,v}$  (concrete edge failure) a concrete cover of the edge reinforcement  $c = 30$  mm is assumed
- Drilled hole cleaning must be performed according to instructions for use (blow twice with oil-free compressed air (min. 6 bar), brush twice, blow twice with oil-free compressed air (min. 6 bar)).
- Characteristic bond resistances depend on short- and long-term temperatures.
- Edge reinforcement is not required to avoid splitting failure
- The characteristic bond resistances depend on the return period (service life in years): 50

**Fastening meets the design criteria!**

## 8 Installation data

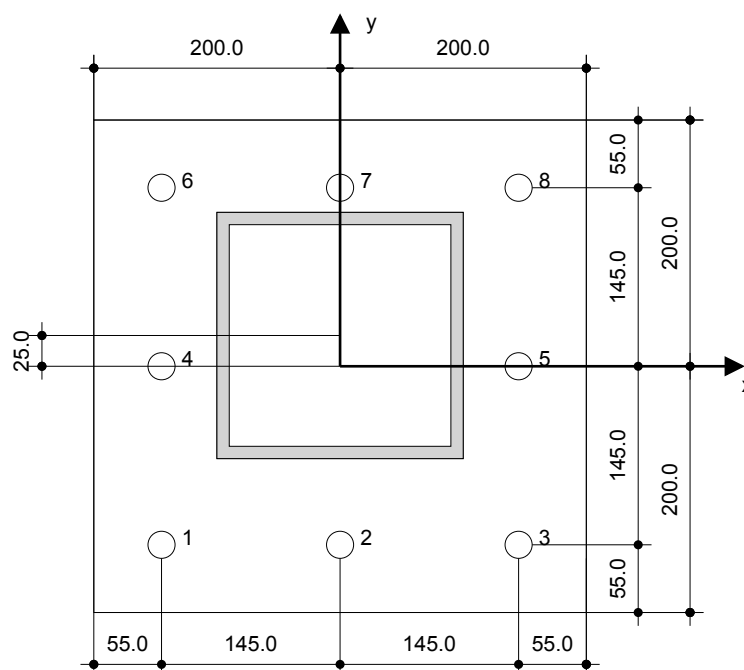
Baseplate, steel: S 275;  $E = 210,000.00 \text{ N/mm}^2$ ;  $f_{yk} = 275.00 \text{ N/mm}^2$   
 Profile: Square hollow, 200 x 200 x 10,0; (L x W x T) = 200.0 mm x 200.0 mm x 10.0 mm  
 Hole diameter in the fixture:  $d_f = 22.0 \text{ mm}$   
 Plate thickness (input): 35.0 mm  
 Recommended plate thickness: not calculated  
 Drilling method: Hammer drilled  
 Cleaning: Compressed air cleaning of the drilled hole according to instructions for use is required

Anchor type and size: HIT-HY 200-A + HAS-U A4 M20  
 Item number: 2223929 HAS-U A4 M20x350 (insert) / 2022696 HIT-HY 200-A (mortar)  
 Installation torque: 150 Nm  
 Hole diameter in the base material: 22.0 mm  
 Hole depth in the base material: 200.0 mm  
 Minimum thickness of the base material: 244.0 mm

Hilti HAS-U threaded rod with HIT-HY 200 injection mortar with 200 mm embedment  $h_{ef}$ , M20, Stainless steel, SAFEsset Auto cleaning Hammer drilling installation per ETA 11/0493

### 8.1 Recommended accessories

Drilling	Cleaning	Setting
<ul style="list-style-type: none"> <li>Suitable Rotary Hammer</li> <li>Properly sized drill bit</li> </ul>	<ul style="list-style-type: none"> <li>Compressed air with required accessories to blow from the bottom of the hole</li> <li>Proper diameter wire brush</li> </ul>	<ul style="list-style-type: none"> <li>Dispenser including cassette and mixer</li> <li>Torque wrench</li> </ul>



Coordinates Anchor mm

Anchor	x	y	c <sub>-x</sub>	c <sub>+x</sub>	c <sub>-y</sub>	c <sub>+y</sub>	Anchor	x	y	c <sub>-x</sub>	c <sub>+x</sub>	c <sub>-y</sub>	c <sub>+y</sub>
1	-145.0	-145.0	-	-	-	-	5	145.0	0.0	-	-	-	-
2	0.0	-145.0	-	-	-	-	6	-145.0	145.0	-	-	-	-
3	145.0	-145.0	-	-	-	-	7	0.0	145.0	-	-	-	-
4	-145.0	0.0	-	-	-	-	8	145.0	145.0	-	-	-	-

## 9 Alternative fastening

### 9.1 Alternative fastening data

<b>Anchor type and size:</b>	<b>HVU2 + HAS-U A4 M20</b>
Return period (service life in years):	50
Item number:	2223928 HAS-U A4 M20x300 (insert) / 2164509 HVU2 M20x170 (capsule)
Effective embedment depth:	$h_{ef,act} = 170.0 \text{ mm}$ , $h_{nom} = 170.0 \text{ mm}$
Material:	A4
Approval No.:	ETA-16/0515
Issued   Valid:	13/11/2019   -
Proof:	Design Method EN 1992-4, Chemical
Stand-off installation:	without clamping (anchor); restraint level (baseplate): 2.00; $e_b = 35.0 \text{ mm}$ ; $t = 35.0 \text{ mm}$
Baseplate <sup>R</sup> :	Hilti Grout: , multipurpose, $f_{c,Grout} = 30.00 \text{ N/mm}^2$ $l_x \times l_y \times t = 400.0 \text{ mm} \times 400.0 \text{ mm} \times 35.0 \text{ mm}$ ; (Recommended plate thickness: not calculated)
Profile:	Square hollow, 200 x 200 x 10,0; (L x W x T) = 200.0 mm x 200.0 mm x 10.0 mm
Base material:	cracked concrete, C40/50, $f_{c,cyl} = 40.00 \text{ N/mm}^2$ ; $h = 365.0 \text{ mm}$ , Temp. short/long: 0/0 °C
<b>Installation:</b>	<b>hammer drilled hole, Installation condition: Dry</b>
Reinforcement:	No reinforcement or Reinforcement spacing $\geq 150 \text{ mm}$ (any $\emptyset$ ) or $\geq 100 \text{ mm}$ ( $\emptyset \leq 10 \text{ mm}$ ) no longitudinal edge reinforcement



## Max. Utilisation with HVU2 + HAS-U A4 M20: 92 % Fastening meets the design criteria!

### 9.2 Installation data

Baseplate, steel: S 275; $E = 210,000.00 \text{ N/mm}^2$ ; $f_{yk} = 275.00 \text{ N/mm}^2$	Anchor type and size: HVU2 + HAS-U A4 M20
Profile: Square hollow, 200 x 200 x 10,0; (L x W x T) = 200.0 mm x 200.0 mm x 10.0 mm	Item number: 2223928 HAS-U A4 M20x300 (insert) / 2164509 HVU2 M20x170 (capsule)
Hole diameter in the fixture: $d_f = 22.0 \text{ mm}$	Installation torque: 150 Nm
Plate thickness (input): 35.0 mm	Hole diameter in the base material: 22.0 mm
Recommended plate thickness: not calculated	Hole depth in the base material: 170.0 mm
Drilling method: Hammer drilled	Minimum thickness of the base material: 220.0 mm
Cleaning: Compressed air cleaning of the drilled hole according to instructions for use is required	

Hilti HAS-U threaded rod with HVU2 capsule mortar with 170 mm embedment  $h_{ef}$ , M20, Stainless steel, SAFESet Auto cleaning Hammer drilling installation per ETA-16/0515

### 9.2.1 Recommended accessories

Drilling	Cleaning	Setting
<ul style="list-style-type: none"> <li>• Suitable Rotary Hammer</li> <li>• Properly sized drill bit</li> </ul>	<ul style="list-style-type: none"> <li>• Compressed air with required accessories to blow from the bottom of the hole</li> <li>• Proper diameter wire brush</li> </ul>	<ul style="list-style-type: none"> <li>• HVA square drive shafts</li> <li>• Torque wrench</li> </ul>



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Company:		Page:	12
Address:		Specifier:	
Phone I Fax:		E-Mail:	
Design:	TEST	Date:	22/05/2020
Fastening Point:	Base plate		

## 10 Remarks; Your Cooperation Duties

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