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Specifier's comments:

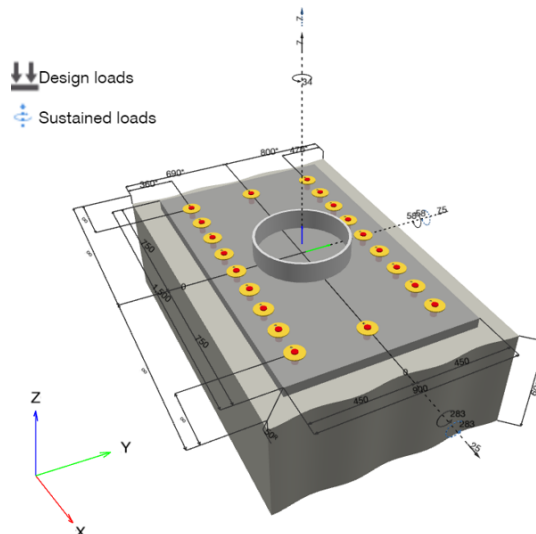
1 Input data

Anchor type and size:	HIT-RE 500 V3 + HAS-U 8.8 HDG M30	
Return period (service life in years):	50	
Item number:	not available (insert) / 2123403 HIT-RE 500 V3 (mortar)	
Hilti Filling Set or any suitable annular gap filling solution		
Effective embedment depth:	$h_{ef,act} = 320.0 \text{ mm}$ ($h_{ef,limit} = - \text{ mm}$)	
Material:	8.8	
Approval No.:	ETA 16/0143	
Issued Valid:	14/5/2019 -	
Proof:	Engineering judgement SOFA BOND - based on ETAG BOND testing	
Stand-off installation:	$e_b = 0.0 \text{ mm}$ (no stand-off); $t = 50.0 \text{ mm}$	
Baseplate ^R :	$l_x \times l_y \times t = 1,500.0 \text{ mm} \times 900.0 \text{ mm} \times 50.0 \text{ mm}$; (Recommended plate thickness: not calculated)	
Profile:	Circular hollow section, 457x12.7CHS; (L x W x T) = 457.0 mm x 457.0 mm x 12.7 mm	
Base material:	uncracked concrete, 50MPa, $f_{c,cube} = 60.00 \text{ N/mm}^2$; $h = 600.0 \text{ mm}$, Temp. short/long: 0/0 °C	
Installation:	automatic cleaned drilled hole, Installation condition: Dry	
Reinforcement:	Reinforcement spacing < 150 mm (any \emptyset) or < 100 mm ($\emptyset \leq 10 \text{ mm}$) with longitudinal edge reinforcement $d \geq 12.0 \text{ [mm]}$ + close mesh (stirrups, hangers) $s \leq 100.0 \text{ [mm]}$ Reinforcement to control splitting according to EOTA TR 029, 5.2.2.6 present.	

Application also possible with HVU2 + HAS-U 8.8 HDG M30 under the selected boundary conditions. More information in section Alternative fastening data of this report.

^R - The anchor calculation is based on a rigid baseplate assumption.

Geometry [mm] & Loading [kN, kNm]



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1.1 Load combination

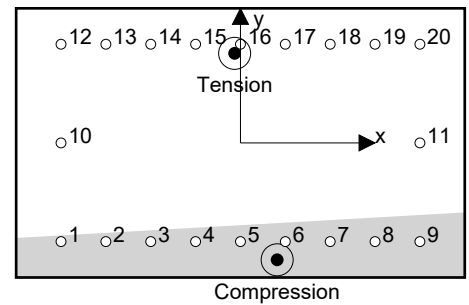
Case	Description	Forces [kN] / Moments [kNm]	Seismic	Fire	Max. Util. Anchor [%]
1	dnm	N = 7.000; V _x = 25.000; V _y = -75.000; M _x = 283.000; M _y = 58.000; M _z = 34.000;	no	no	57

2 Load case/Resulting anchor forces

Anchor reactions [kN]

Tension force: (+Tension, -Compression)

Anchor	Tension force	Shear force	Shear force x	Shear force y
1	0.000	8.246	3.335	-7.542
2	0.000	7.389	3.335	-6.594
3	0.000	6.557	3.335	-5.646
4	0.000	5.762	3.335	-4.698
5	0.000	5.019	3.335	-3.750
6	0.000	4.356	3.335	-2.802
7	0.000	3.816	3.335	-1.854
8	0.000	3.456	3.335	-0.906
9	0.000	3.336	3.335	0.042
10	21.481	7.645	1.250	-7.542
11	16.805	1.251	1.250	0.042
12	44.073	7.588	-0.835	-7.542
13	43.489	6.646	-0.835	-6.594
14	42.904	5.707	-0.835	-5.646
15	42.320	4.772	-0.835	-4.698
16	41.735	3.842	-0.835	-3.750
17	41.150	2.924	-0.835	-2.802
18	40.566	2.034	-0.835	-1.854
19	39.981	1.233	-0.835	-0.906
20	39.397	0.836	-0.835	0.042



max. concrete compressive strain: 0.13 [‰]
 max. concrete compressive stress: 3.90 [N/mm²]
 resulting tension force in (x/y)=(-19.5/299.5): 413.901 [kN]
 resulting compression force in (x/y)=(122.7/-390.9): 406.901 [kN]

Anchor forces are calculated based on the assumption of a rigid baseplate.

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3 Tension load (EOTA TR 029, Section 5.2.2)

	Load [kN]	Capacity [kN]	Utilization β_N [%]	Status
Steel failure*	44.073	299.200	15	OK
Combined pullout-concrete cone failure**	413.901	894.452	47	OK
Concrete Breakout failure**	413.901	782.782	53	OK
Splitting failure**	413.901	1,188.894	35	OK

* highest loaded anchor **anchor group (anchors in tension)

3.1 Steel failure

$N_{Rk,s}$ [kN]	$\gamma_{M,s}$	$N_{Rd,s}$ [kN]	N_{Sd} [kN]
448.800	1.500	299.200	44.073

3.2 Combined pullout-concrete cone failure

$A_{p,N}$ [mm ²]	$A_{p,N}^0$ [mm ²]	$\tau_{Rk,ucr,25}$ [N/mm ²]	$s_{cr,Np}$ [mm]	$c_{cr,Np}$ [mm]	c_{min} [mm]
2,196,746	672,000	14.00	819.8	409.9	470.0
Ψ_c	$\tau_{Rk,ucr}$ [N/mm ²]	k	$\Psi_{g,Np}^0$	$\Psi_{g,Np}$	
1.091	15.28	3.200	1.000	1.000	
$e_{c1,N}$ [mm]	$\Psi_{ec1,Np}$	$e_{c2,N}$ [mm]	$\Psi_{ec2,Np}$	$\Psi_{s,Np}$	$\Psi_{re,Np}$
19.5	0.955	29.5	0.933	1.000	1.000
$N_{Rk,p}^0$ [kN]	$N_{Rk,p}$ [kN]	$\gamma_{M,p}$	$N_{Rd,p}$ [kN]	N_{Sd} [kN]	
460.861	1,341.678	1.500	894.452	413.901	

Group anchor ID

10-20

3.3 Concrete Breakout failure

$A_{c,N}$ [mm ²]	$A_{c,N}^0$ [mm ²]	$c_{cr,N}$ [mm]	$s_{cr,N}$ [mm]		
2,685,600	921,600	480.0	960.0		
$e_{c1,N}$ [mm]	$\Psi_{ec1,N}$	$e_{c2,N}$ [mm]	$\Psi_{ec2,N}$	$\Psi_{s,N}$	$\Psi_{re,N}$
19.5	0.961	29.5	0.942	0.994	1.000
k_1	$N_{Rk,c}^0$ [kN]	$\gamma_{M,c}$	$N_{Rd,c}$ [kN]	N_{Sd} [kN]	
10.100	447.839	1.500	782.782	413.901	

Group anchor ID

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3.4 Splitting failure

$A_{c,N}$ [mm ²]	$A_{c,N}^0$ [mm ²]	$c_{cr,sp}$ [mm]	$s_{cr,sp}$ [mm]	$\Psi_{h,sp}$		
2,072,896	614,656	392.0	784.0	1.333		
$e_{c1,N}$ [mm]	$\Psi_{ec1,N}$	$e_{c2,N}$ [mm]	$\Psi_{ec2,N}$	$\Psi_{s,N}$	$\Psi_{re,N}$	k_1
19.5	0.953	29.5	0.930	1.000	1.000	10.100
$N_{Rk,c}^0$ [kN]	$\gamma_{M,sp}$	$N_{Rd,sp}$ [kN]	N_{Sd} [kN]			
447.839	1.500	1,188.894	413.901			
Group anchor ID						
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4 Shear load (EOTA TR 029, Section 5.2.3)

	Load [kN]	Capacity [kN]	Utilization β_v [%]	Status
Steel failure (without lever arm)*	8.246	179.520	5	OK
Steel failure (with lever arm)*	N/A	N/A	N/A	N/A
Pryout failure**	79.057	812.435	10	OK
Concrete edge failure in direction y-**	80.901	249.148	33	OK

* highest loaded anchor **anchor group (relevant anchors)

4.1 Steel failure (without lever arm)

V _{Rk,s} [kN]	γ _{M,s}	V _{Rd,s} [kN]	V _{Sd} [kN]
224.400	1.250	179.520	8.246

4.2 Pryout failure (concrete cone relevant)

A _{c,N} [mm ²]	A _{c,N} ⁰ [mm ²]	c _{cr,N} [mm]	s _{cr,N} [mm]	k-factor	
3,218,400	921,600	480.0	960.0	2.000	
e _{c1,v} [mm]	ψ _{ec1,N}	e _{c2,v} [mm]	ψ _{ec2,N}	ψ _{s,N}	ψ _{re,N}
408.0	0.541	136.0	0.779	0.925	1.000
N _{Rk,c} ⁰ [kN]	γ _{M,c,p}	V _{Rd,op} [kN]	V _{Sd} [kN]		
447.839	1.500	812.435	79.057		

Group anchor ID

1-20

4.3 Concrete edge failure in direction y-

l _f [mm]	d _{nom} [mm]	k ₁	α	β	
320.0	30.00	2.400	0.094	0.061	
c ₁ [mm]	A _{c,v} [mm ²]	A _{c,v} ⁰ [mm ²]			
360.0	1,231,200	583,200			
ψ _{s,v}	ψ _{h,v}	ψ _{α,v}	e _{c,v} [mm]	ψ _{ec,v}	ψ _{re,v}
1.000	1.000	1.063	266.2	0.670	1.000
V _{Rk,c} ⁰ [kN]	γ _{M,c}	V _{Rd,c} [kN]	V _{Sd} [kN]		
248.547	1.500	249.148	80.901		

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5 Combined tension and shear loads (EOTA TR 029, Section 5.2.4)

Steel failure

β_N	β_V	α_N	α_V	Utilization $\beta_{N,V}$ [%]	Status
0.529	0.325	1.500	0.000	57	OK

$$\beta_N^{\alpha_N} + \beta_V^{\alpha_V} \leq 1.0$$

6 Displacements (highest loaded anchor)

Short term loading:

N_{Sk}	=	32.647 [kN]	δ_N	=	0.0866 [mm]
V_{Sk}	=	5.621 [kN]	δ_V	=	0.1686 [mm]
			δ_{NV}	=	0.1896 [mm]

Long term loading:

N_{Sk}	=	32.647 [kN]	δ_N	=	0.2057 [mm]
V_{Sk}	=	5.621 [kN]	δ_V	=	0.2810 [mm]
			δ_{NV}	=	0.3483 [mm]

Comments: Tension displacements are valid with half of the required installation torque moment for uncracked concrete! Shear displacements are valid without friction between the concrete and the baseplate! The gap due to the drilled hole and clearance hole tolerances are not included in this calculation!

The acceptable anchor displacements depend on the fastened construction and must be defined by the designer!

7 Warnings

- The anchor design methods in PROFIS Engineering require rigid baseplates per current regulations (AS 5216:2021, ETAG 001/Annex C, EOTA TR029 etc.). This means load re-distribution on the anchors due to elastic deformations of the baseplate are not considered - the baseplate is assumed to be sufficiently stiff, in order not to be deformed when subjected to the design loading. PROFIS Engineering calculates the minimum required baseplate thickness with CBFEM to limit the stress of the baseplate based on the assumptions explained above. The proof if the rigid baseplate assumption is valid is not carried out by PROFIS Engineering. Input data and results must be checked for agreement with the existing conditions and for plausibility!
- Checking the transfer of loads into the base material is required in accordance with EOTA TR 029, Section 7!
- The design is only valid if the clearance hole in the fixture is not larger than the value given in Table 4.1 of EOTA TR029! For larger diameters of the clearance hole see Chapter 1.1. of EOTA TR029!
- Your design has selected filled holes. Please ensure that there is a proper method to fill the annular gap between the fixture and HIT-RE 500 V3 + HAS-U 8.8 HDG M30 and contact Hilti in case of any questions.
- The accessory list in this report is for the information of the user only. In any case, the instructions for use provided with the product have to be followed to ensure a proper installation.
- Characteristic bond resistances depend on short- and long-term temperatures.
- The design method SOFA assumes that no hole clearance between the anchors and the fixture is present. This can be achieved by filling the gap with mortar of sufficient compressive strength (e.g. by using the HILTI Filling set) or by other suitable means
- The compliance with current standards (e.g. EN 1993, AS 4100:1998, etc.) is the responsibility of the user
- An SLS-check is not performed for SOFA and has to be provided by the user!
- The characteristic bond resistances depend on the return period (service life in years): 50



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Fastening meets the design criteria!

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8 Installation data

Baseplate, steel: Grade 300; $E = 200,000.00 \text{ N/mm}^2$; $f_{yk} = 280.00 \text{ N/mm}^2$

Profile: Circular hollow section, 457x12.7CHS; $(L \times W \times T) = 457.0 \text{ mm} \times 457.0 \text{ mm} \times 12.7 \text{ mm}$

Hole diameter in the fixture: $d_f = 33.0 \text{ mm}$

Plate thickness (input): 50.0 mm

Recommended plate thickness: not calculated

Drilling method: SafeSet - automatic cleaning

Cleaning: Automatically performed while drilling

Anchor type and size: HIT-RE 500 V3 + HAS-U 8.8 HDG M30

Item number: not available (insert) / 2123403 HIT-RE 500 V3 (mortar)

Maximum installation torque: 300 Nm

Hole diameter in the base material: 35.0 mm

Hole depth in the base material: 320.0 mm

Minimum thickness of the base material: 390.0 mm

Hilti HAS-U threaded rod with HIT-RE 500 V3 injection mortar with 320 mm embedment h_{ef} , M30, Hot dip galvanized, SAFEset - automatic cleaning installation per ETA 16/0143, with annular gaps filled with Hilti Filling Set or any suitable gap solutions

8.1 Recommended accessories

Drilling

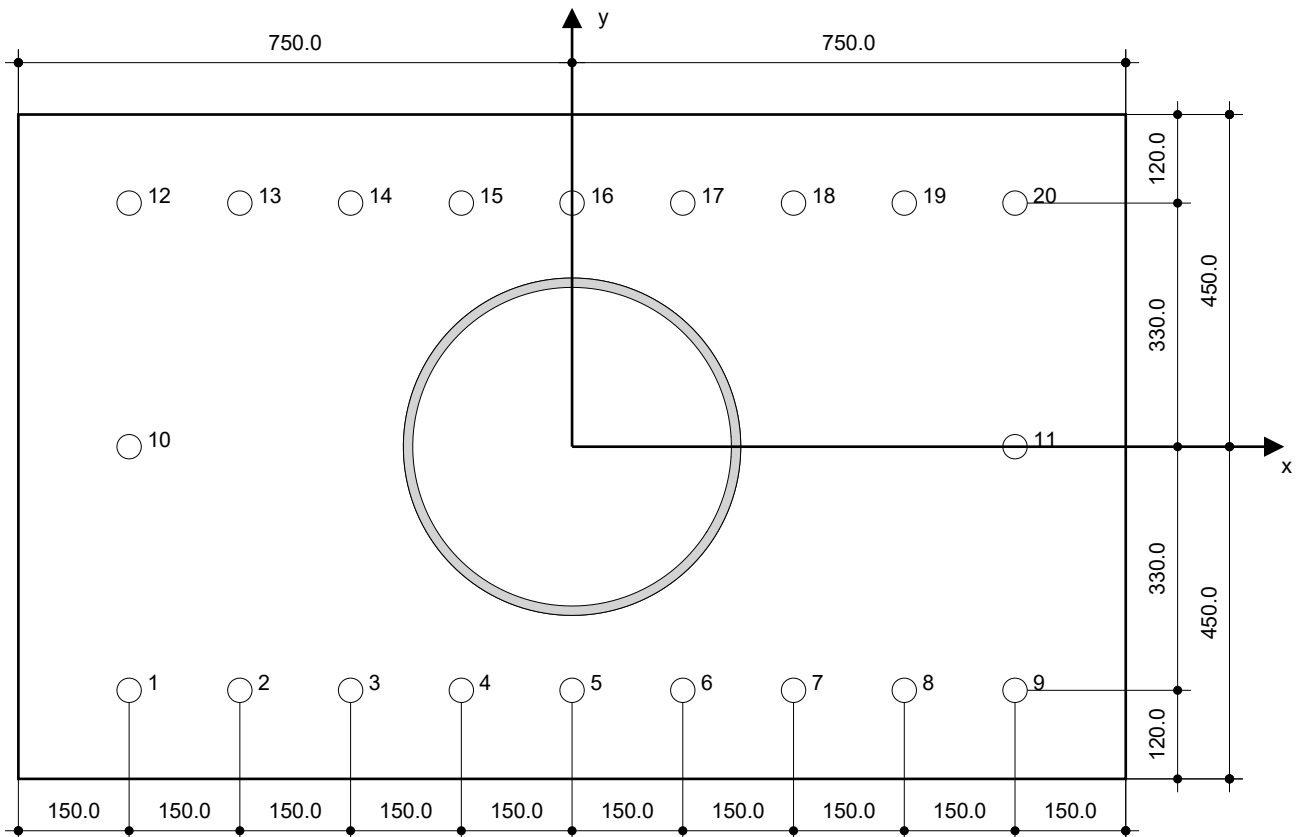
- Suitable Rotary Hammer
- Properly sized drill bit for SAFEset - automatic cleaning (TE-CD / TE-YD)
- Vacuum cleaner

Cleaning

- No accessory required

Setting

- Dispenser including cassette and mixer
- Hilti Filling Set
- Torque wrench





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Coordinates Anchor [mm]

Anchor	x	y	C _{-x}	C _{+x}	C _{-y}	C _{+y}	Anchor	x	y	C _{-x}	C _{+x}	C _{-y}	C _{+y}
1	-600.0	-330.0	-	-	360.0	1,130.0	11	600.0	0.0	-	-	690.0	800.0
2	-450.0	-330.0	-	-	360.0	1,130.0	12	-600.0	330.0	-	-	1,020.0	470.0
3	-300.0	-330.0	-	-	360.0	1,130.0	13	-450.0	330.0	-	-	1,020.0	470.0
4	-150.0	-330.0	-	-	360.0	1,130.0	14	-300.0	330.0	-	-	1,020.0	470.0
5	0.0	-330.0	-	-	360.0	1,130.0	15	-150.0	330.0	-	-	1,020.0	470.0
6	150.0	-330.0	-	-	360.0	1,130.0	16	0.0	330.0	-	-	1,020.0	470.0
7	300.0	-330.0	-	-	360.0	1,130.0	17	150.0	330.0	-	-	1,020.0	470.0
8	450.0	-330.0	-	-	360.0	1,130.0	18	300.0	330.0	-	-	1,020.0	470.0
9	600.0	-330.0	-	-	360.0	1,130.0	19	450.0	330.0	-	-	1,020.0	470.0
10	-600.0	0.0	-	-	690.0	800.0	20	600.0	330.0	-	-	1,020.0	470.0

9 Alternative fastening

9.1 Alternative fastening data

Anchor type and size: HVU2 + HAS-U 8.8 HDG M30

Return period (service life in years): 50

Item number: 2223918 HAS-U 8.8 HDG M30x380 (insert) /
2164562 HVU2 M30x270 (capsule)



Hilti Filling Set or any suitable annular gap filling solution

Effective embedment depth: $h_{ef,act} = 270.0$ mm, $h_{nom} = 270.0$ mm

Material: 8.8

Approval No.: ETA-16/0515

Issued | Valid: 23/8/2022 | -

Proof: Engineering judgement SOFA BOND - based on ETAG BOND testing

Stand-off installation: $e_b = 0.0$ mm (no stand-off); $t = 50.0$ mm

Baseplate^R: $l_x \times l_y \times t = 1,500.0$ mm x 900.0 mm x 50.0 mm; (Recommended plate thickness: not calculated)

Profile: Circular hollow section, 457x12.7CHS; (L x W x T) = 457.0 mm x 457.0 mm x 12.7 mm

Base material: uncracked concrete, 50MPa, $f_{c,cube} = 60.00$ N/mm²; $h = 600.0$ mm, Temp. short/long: 0/0 °C

Installation: automatic cleaned drilled hole, Installation condition: Dry

Reinforcement: Reinforcement spacing < 150 mm (any \emptyset) or < 100 mm ($\emptyset \leq 10$ mm)
with longitudinal edge reinforcement $d \geq 12.0$ [mm] + close mesh (stirrups, hangers) $s \leq 100.0$ [mm]
Reinforcement to control splitting according to EOTA TR 029, 5.2.2.6 present.

**Max. Utilisation with HVU2 + HAS-U 8.8 HDG M30: 68 %
Fastening meets the design criteria!**

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9.2 Installation data

Baseplate, steel: Grade 300; $E = 200,000.00 \text{ N/mm}^2$; $f_{yk} = 280.00 \text{ N/mm}^2$

Profile: Circular hollow section, 457x12.7CHS; (L x W x T) = 457.0 mm x 457.0 mm x 12.7 mm

Hole diameter in the fixture: $d_f = 33.0 \text{ mm}$

Plate thickness (input): 50.0 mm

Recommended plate thickness: not calculated

Drilling method: SafeSet - automatic cleaning

Cleaning: Automatically performed while drilling

Anchor type and size: HVU2 + HAS-U 8.8 HDG M30

Item number: 2223918 HAS-U 8.8 HDG M30x380 (insert) / 2164562 HVU2 M30x270 (capsule)

Maximum installation torque: 300 Nm

Hole diameter in the base material: 35.0 mm

Hole depth in the base material: 270.0 mm

Minimum thickness of the base material: 340.0 mm

Hilti HAS-U threaded rod with HVU2 capsule mortar with 270 mm embedment h_{ef} , M30, Hot dip galvanized, SAFEset - automatic cleaning installation per ETA-16/0515, with annular gaps filled with Hilti Filling Set or any suitable gap solutions

9.2.1 Recommended accessories

Drilling	Cleaning	Setting
<ul style="list-style-type: none">• Suitable Rotary Hammer• Properly sized drill bit for SAFEset - automatic cleaning (TE-CD / TE-YD)• Vacuum cleaner	<ul style="list-style-type: none">• No accessory required	<ul style="list-style-type: none">• HVA square drive shafts• Hilti Filling Set• Torque wrench



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10 Remarks; Your Cooperation Duties

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